
Fracture toughness of periodic beam lattices

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Journées d'automne du GDR ARCHI-META, Lille

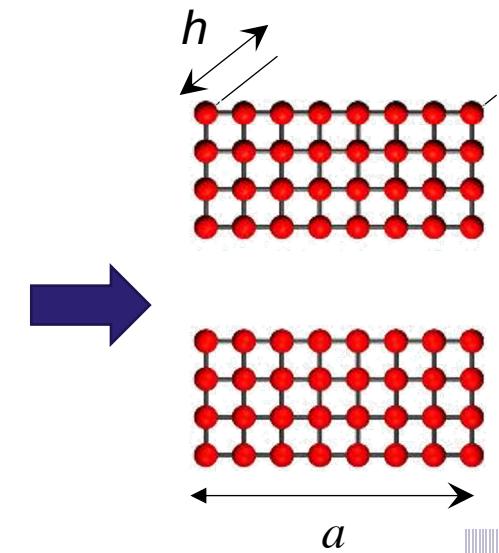
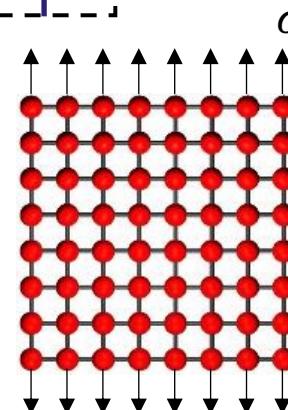
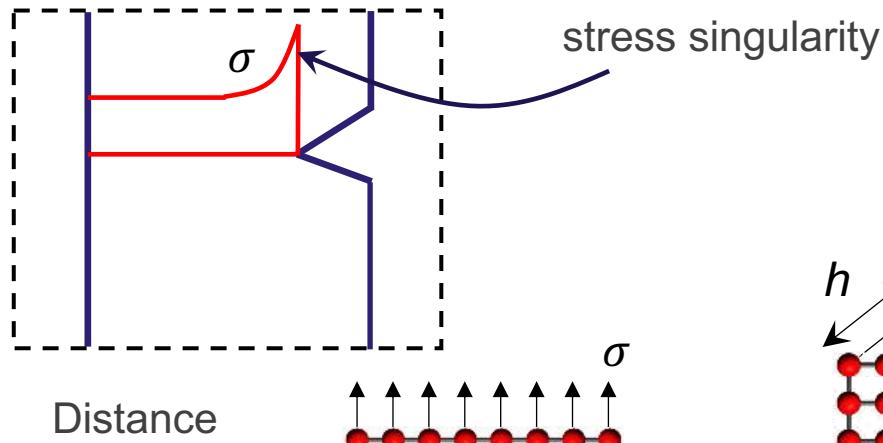
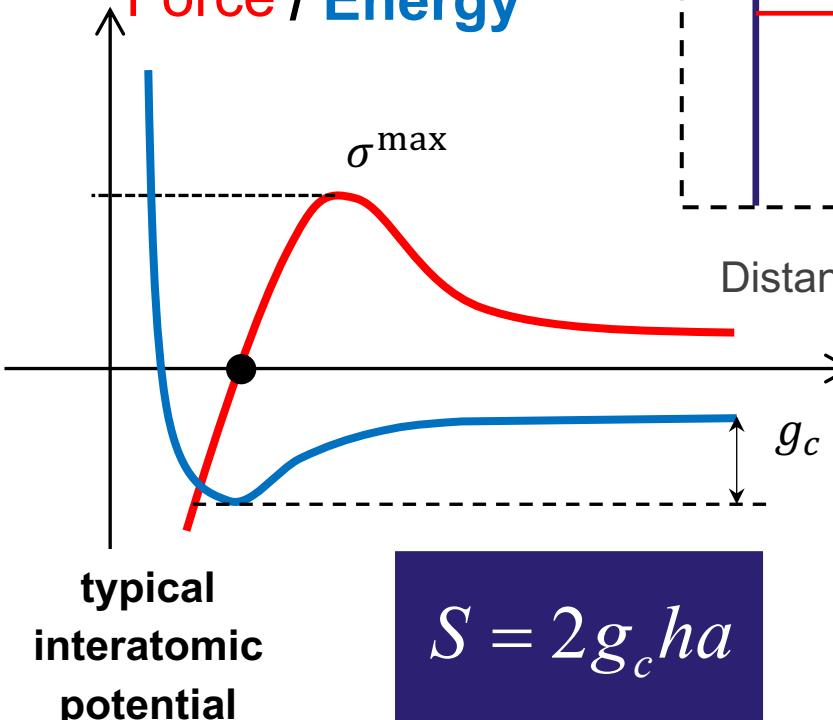
29/11/2024



Motivation

Energy release rate

Force / Energy

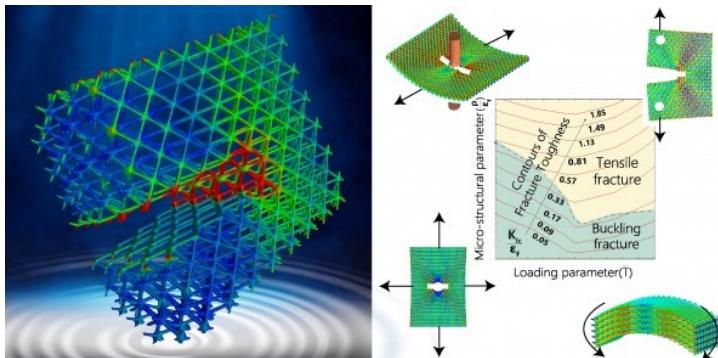


Griffith (1921, 1924)



Motivation

Toughness of metamaterials

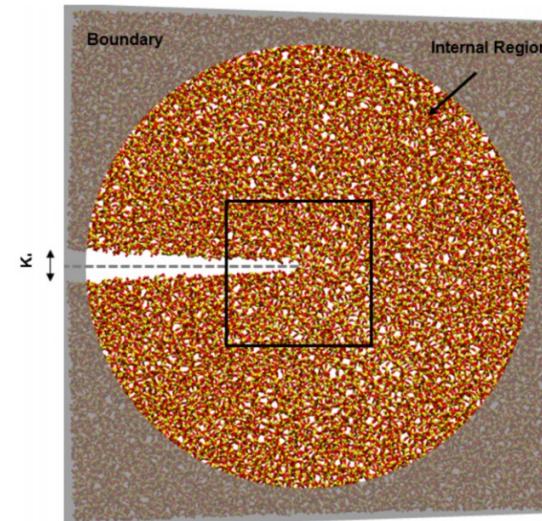


Shaikeea et al. (2022), Nature Materials

Asymptotic analysis:

$$\tilde{\sigma}_{ij} \equiv \frac{\sigma_{ij}}{\sigma_f} = \bar{K}_I \left[\bar{r}^{-\frac{1}{2}} f_{ij}^I + \bar{T}_{11} \delta_{1i} \delta_{1j} + \bar{T}_{33} \delta_{3i} \delta_{3j} + \bar{T}_{13} \delta_{1i} \delta_{3j} + \mathcal{O}(\bar{r}^{\frac{1}{2}}) + \mathcal{O}(\bar{r}) + \dots \right]$$

Toughness of amorphous matter



J integral

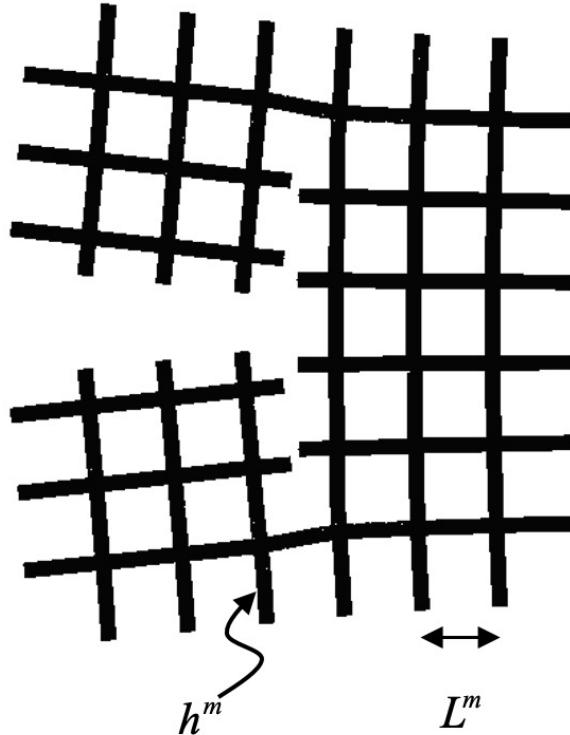
$$J_I = \int_S \left(\Pi_\epsilon n_x - \mathbf{t} \frac{\partial \mathbf{u}}{\partial x} \right) dS$$

QUESTION:
Can we calculate toughness
based on an RVE?

G. Molnár et al.

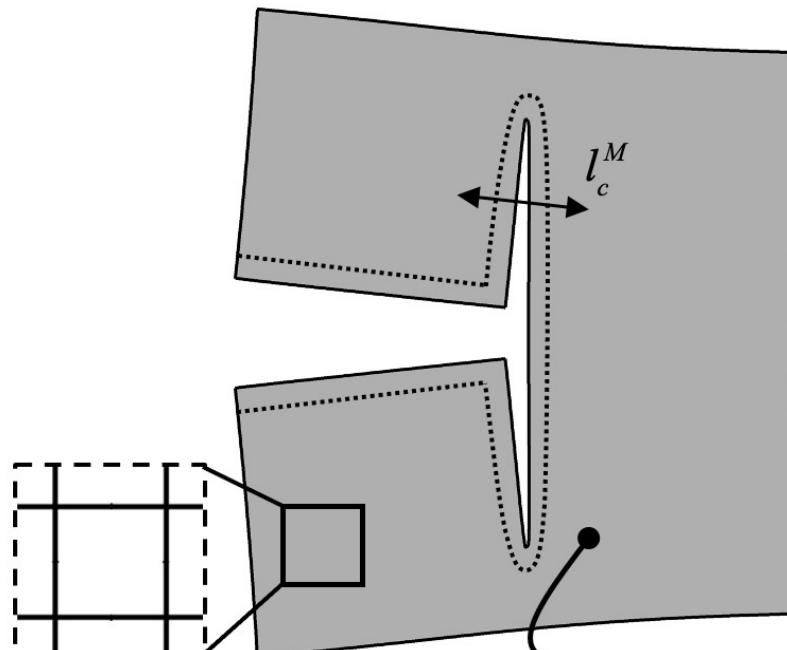
Problem statement

(a) Discrete beam



micro-strength: σ_c^m

(b) Continuum phase-field



macro-toughness: g_c^M

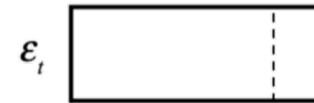
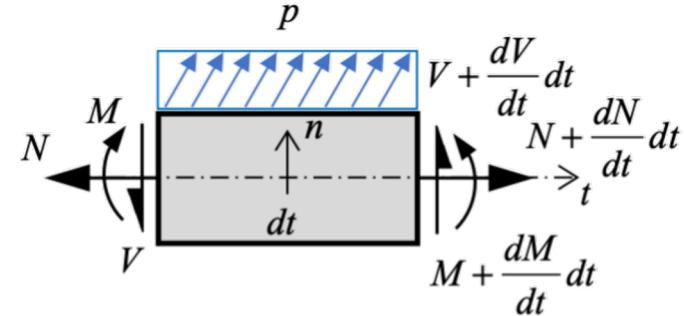
- Critical load
- Fracture topology
- Various loading

Beam model

Euler-Bernoulli beams

Modelling assumptions

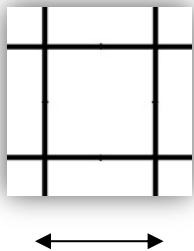
- beams are flawless
- no stress concentration at joints
- $\sigma_t < \sigma_c^m$



Beam model

Toughness calculation

Micro

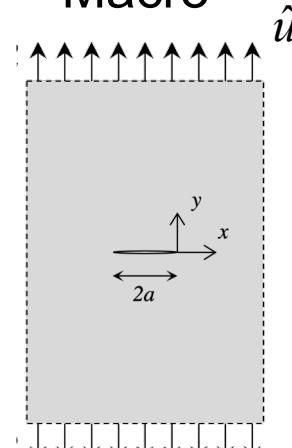


L^m

h^m

σ_c^m

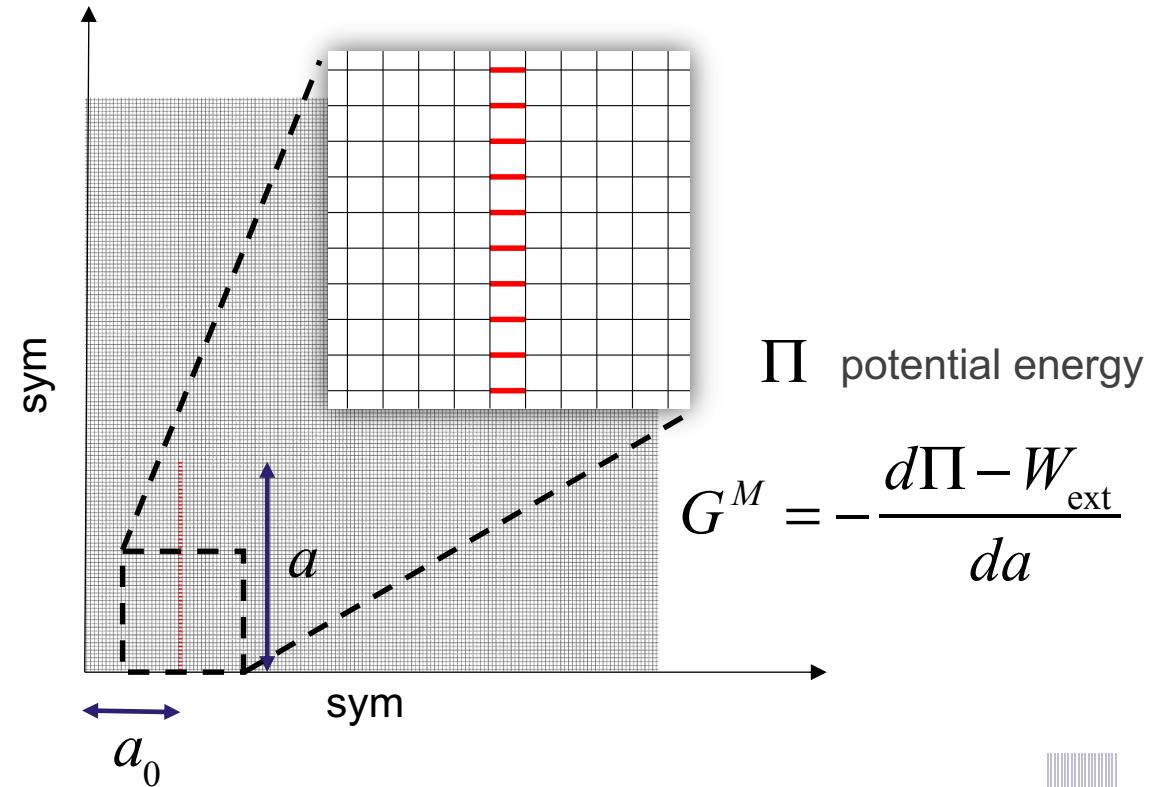
Macro



?

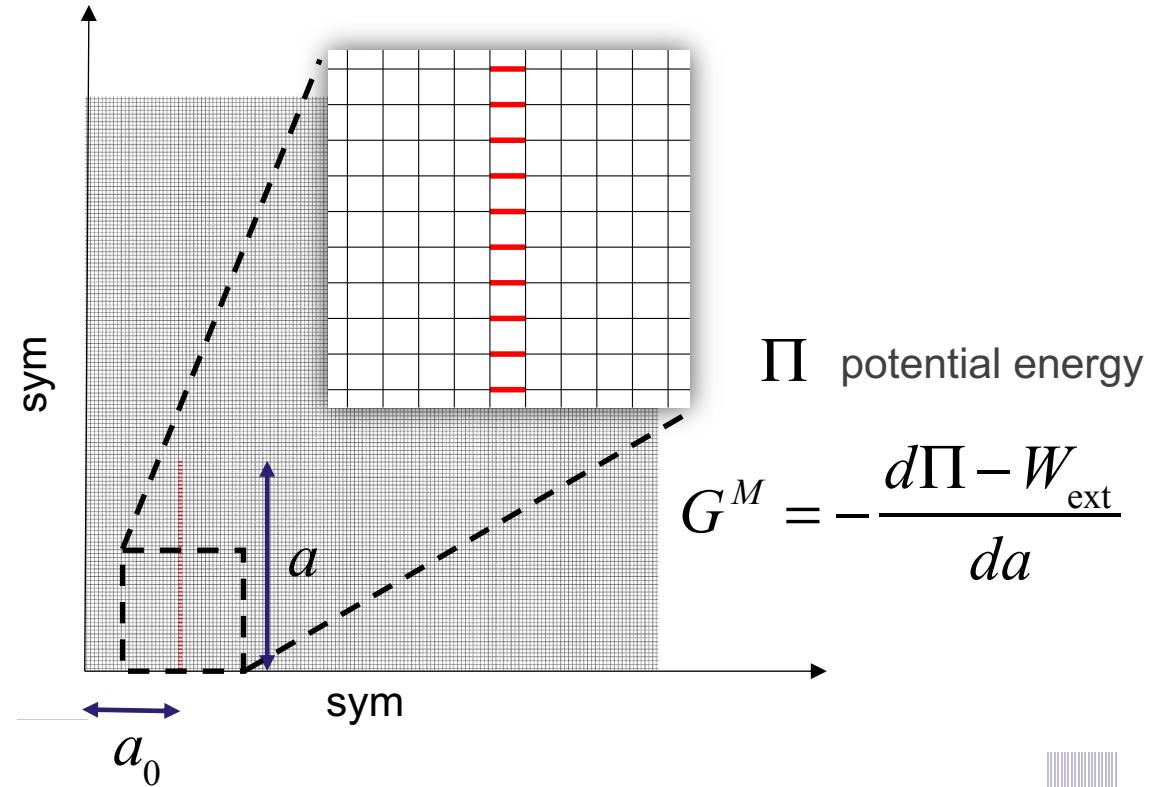
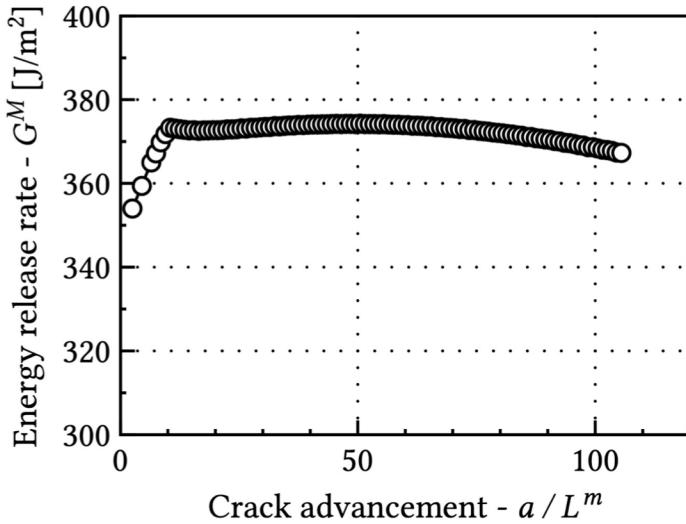
σ_c^M

$g_c^M \approx G^M$



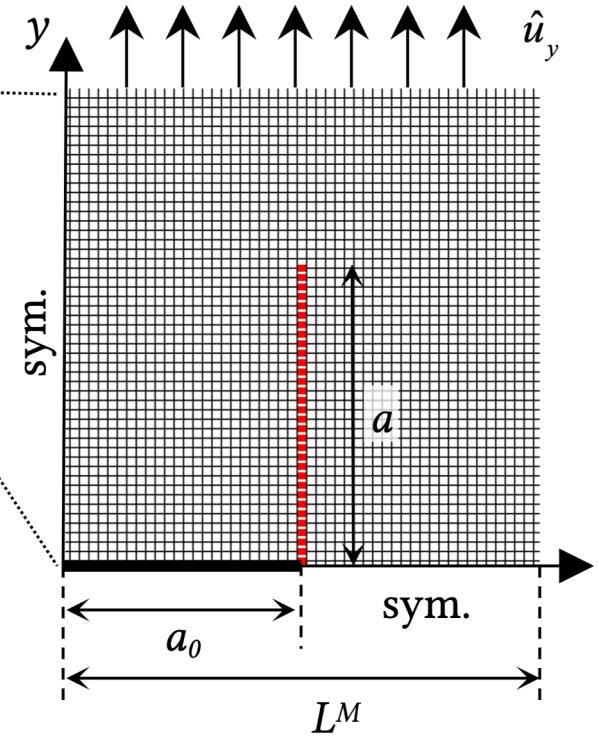
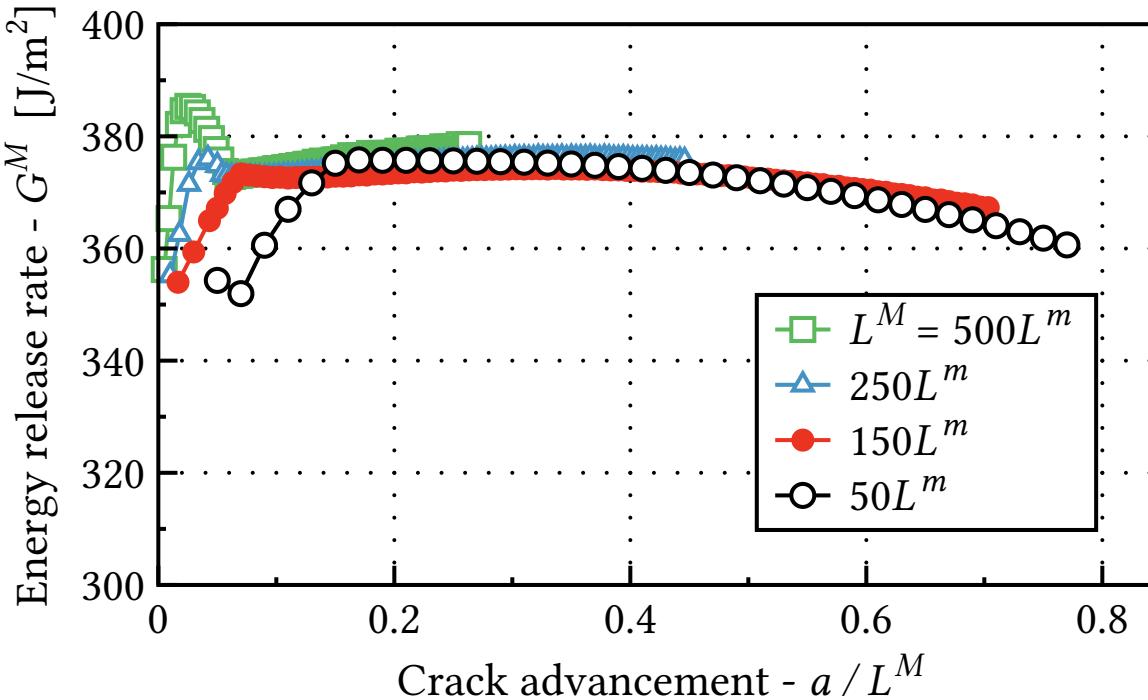
Beam results

Toughness calculation



Beam results

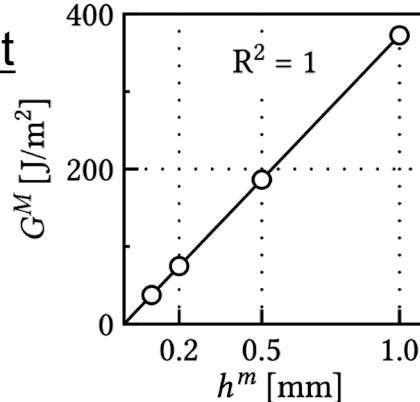
Effect of model geometry



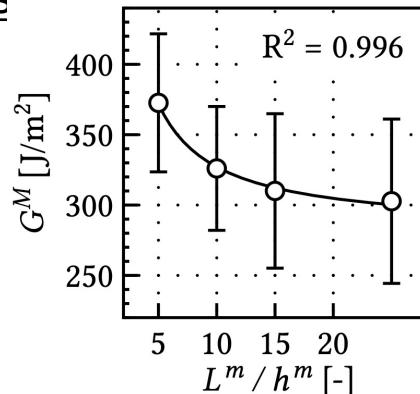
Beam results

Effect of microstructure and material

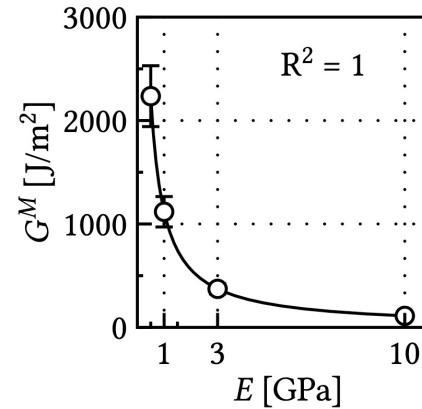
Beam height



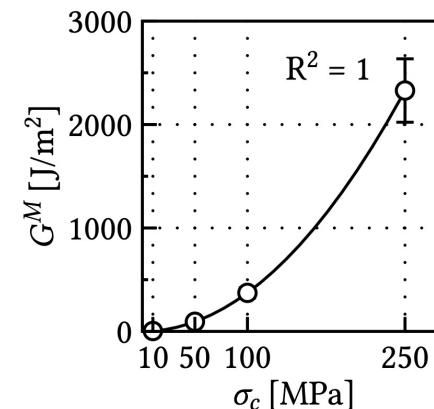
Slenderness



Young's modulus



Strength



$$G^M \sim g_{\text{Irwin}} \approx \frac{\left(\sigma_c^m\right)^2 h^m}{E}$$

Fracture toughness based on RVE?

Continuum model

Phase-field theory

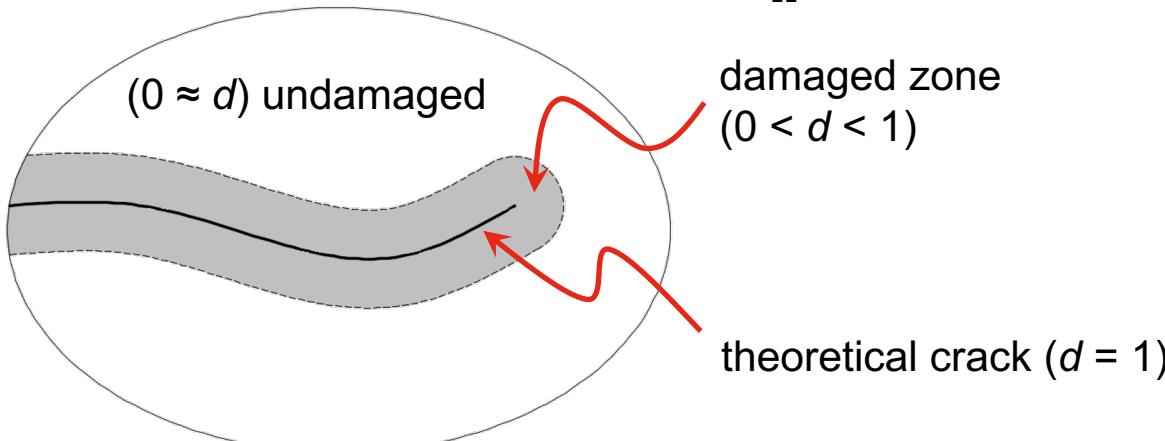
1. Brittle fracture

$$-\frac{\partial \psi}{\partial a} = \frac{\partial S}{\partial a} = \mathbf{g}_c \quad (\text{Griffith, 1920})$$

crack energy
density

2. Minimization problem

$$\Pi(\mathbf{u}, d) = \int_{\Omega} g(d) \psi_0(\varepsilon(\mathbf{u})) d\Omega + \int_{\Omega} \frac{3g_{c,M}}{8l_c^2} \left(d + l_c^2 |\nabla d|^2 \right) d\Omega$$



(Ambrosio & Tortorelli, 1990)
(Bourdin et al., 2000)
(Amor et al., 2009)
(Miehe et al., 2010)

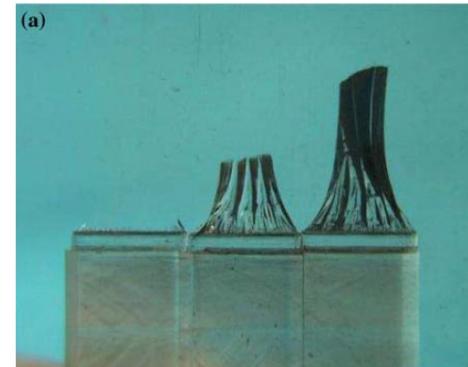
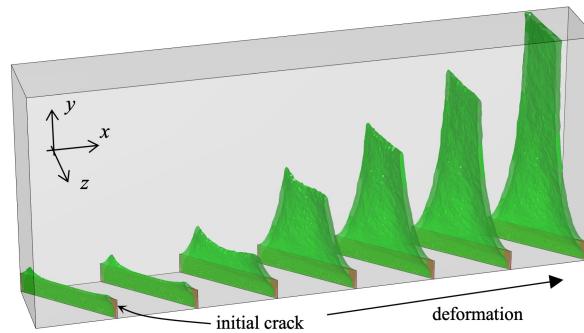
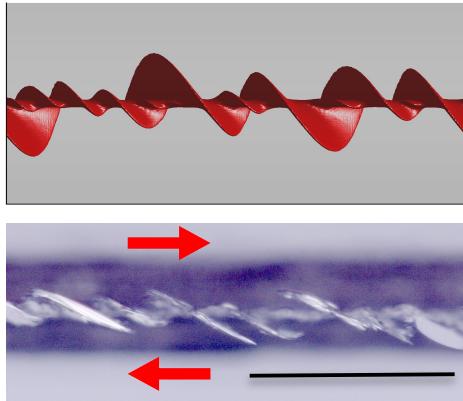
$l_c \rightarrow 0$ Γ converges

Continuum model

Molnár & Gravouil (2017)

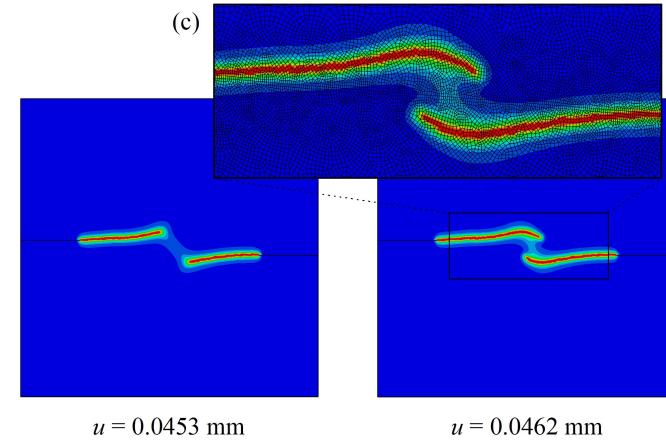
Phase-field examples

Molnár et al. (2024)



Lazarus et al. (2008)

(c)



Mode I+II

G. Molnár et al.

Continuum model

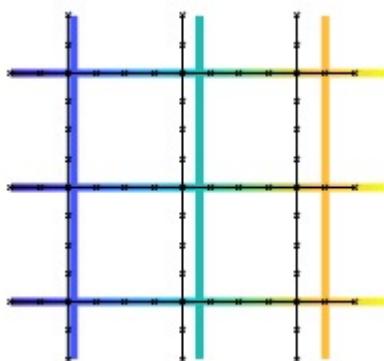


Cosserat theory

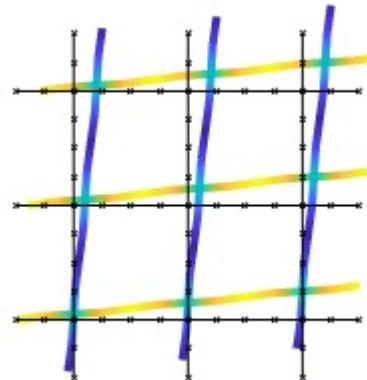
New DOF: rotation ϕ

$$\Pi(\mathbf{u}, \phi, \mathbf{d}) = \int_{\Omega} g(\mathbf{d}) \cdot \psi(\boldsymbol{\varepsilon}(\mathbf{u}, \phi)) \, d\Omega + W(\mathbf{d}, \nabla \mathbf{d})$$

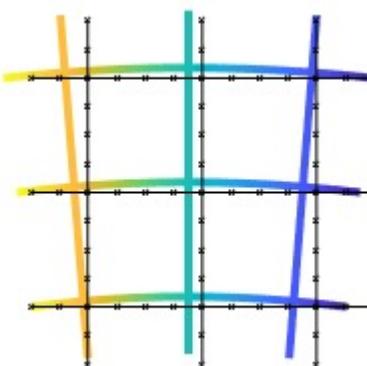
New deformations



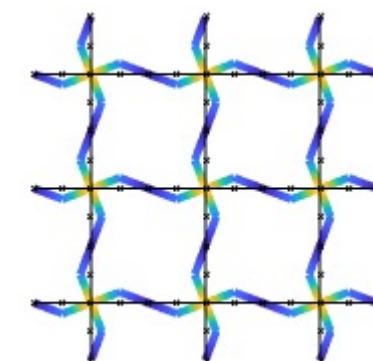
extension



shear



curvature



uniform rotation of joints

(Cosserat & Cosserat, 1909)

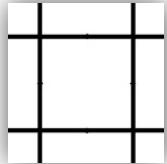


Continuum model

Bleyer & Alessi (2018)
Scherer et al. (2022)

Multiple damage fields

$$\Pi(\mathbf{u}, \mathbf{d}) = \Psi\left(\mathbf{u}, \phi, g_{ij}(\mathbf{d}_i)\right) + \sum_{i=1}^2 \frac{3g_{c,M,i}}{8l_{c,M,i}} \int_{\Omega} \left(\mathbf{d}_i + l_{c,M,i}^2 |\nabla \mathbf{d}_i|^2 \right) d\Omega$$



Degradation functions

$$\Psi\left(\mathbf{u}, \phi, g_{ij}(\mathbf{d}_i)\right) = \frac{1}{2} \int_{\Omega} \underline{\varepsilon}^T \underline{\underline{C}}\left(g_{ij}(\mathbf{d}_i)\right) \underline{\varepsilon} d\Omega$$

$$g_{ij}(\mathbf{d}) = \left(\frac{1 - \mathbf{d}}{1 + \mathbf{d}\gamma_{ij}} \right)^2$$

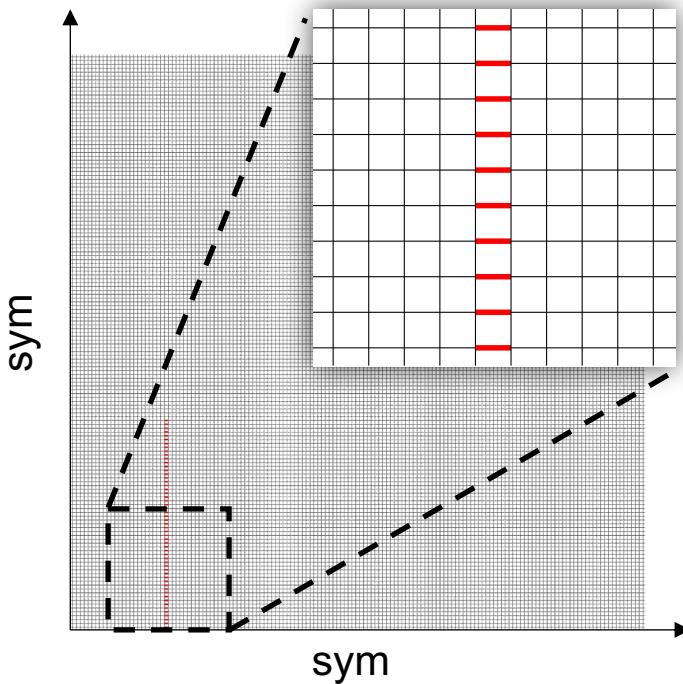
Lorentz & Godard (2011)

$$\underline{\underline{C}} = \begin{bmatrix} g(d_1, \gamma_{11}) C_{11} & & & & & \\ & g(d_2, \gamma_{22}) C_{22} & & & & \emptyset \\ & & g(d_2, \gamma_{23}) C_{33} & & & \\ & & & g(d_1, \gamma_{14}) C_{44} & & \\ & sym. & & & g(d_1, \gamma_{55}) C_{55} & \\ & & & & & g(d_2, \gamma_{66}) C_{66} \end{bmatrix}$$

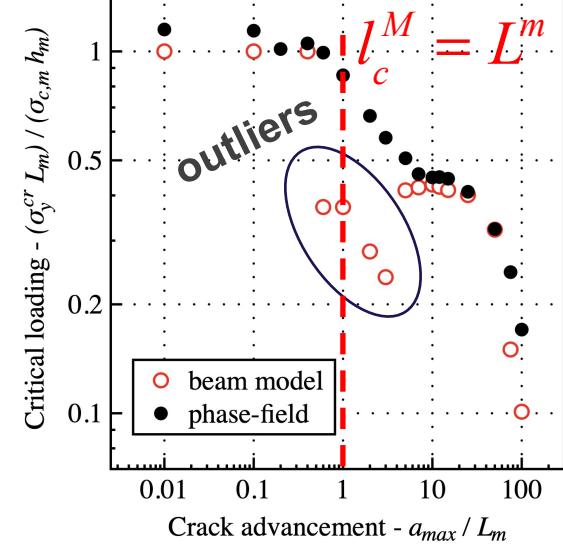
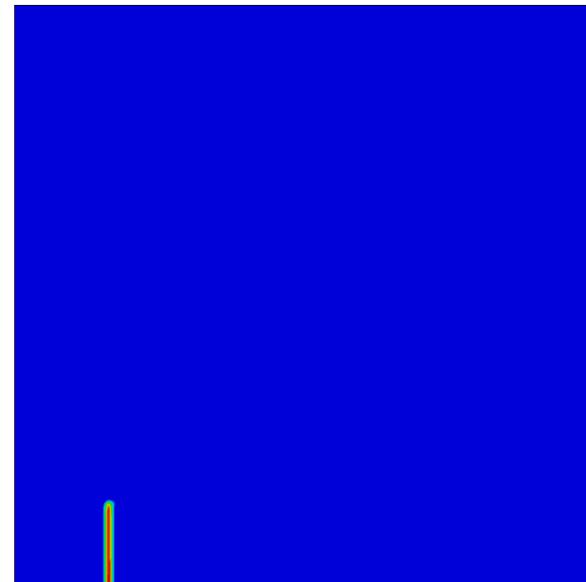
Calibration

Square grid in tension (Mode I)

Beam model



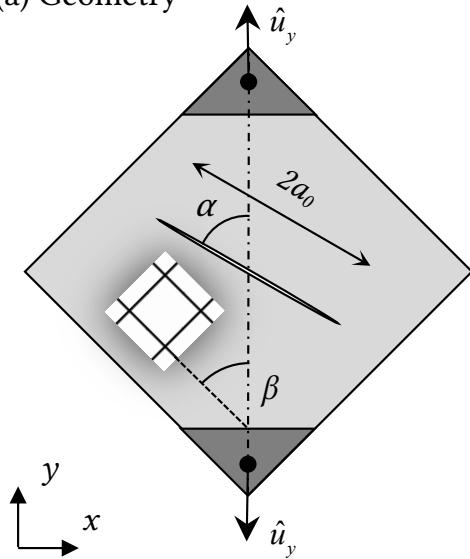
Phase-field



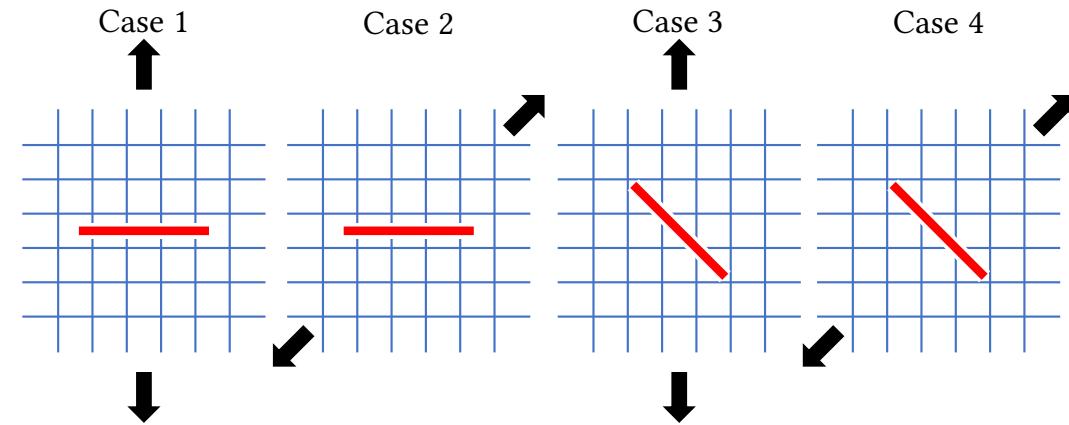
Experimental validation

Principal orientations

(a) Geometry



(b) Orientations

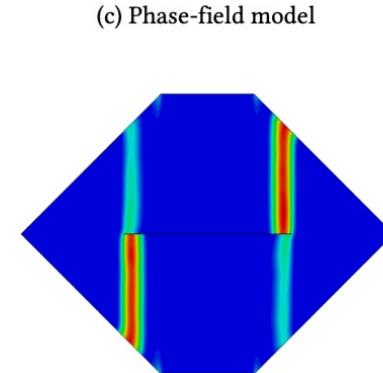
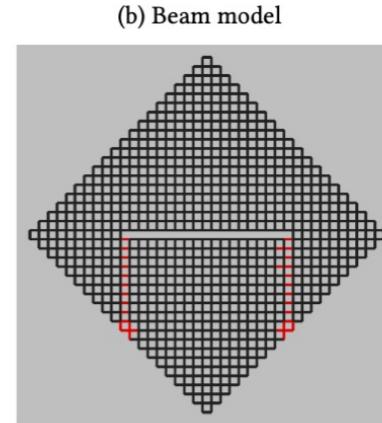
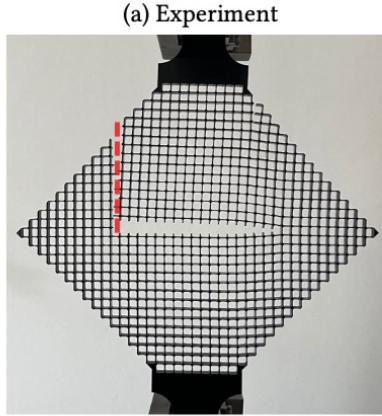


Crack/Loading (α):	90°	45°	45°	90°
Structure/Loading (β):	90°	45°	90°	45°
Crack/Structure :	0°	0°	45°	45°

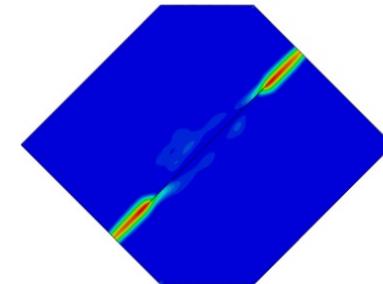
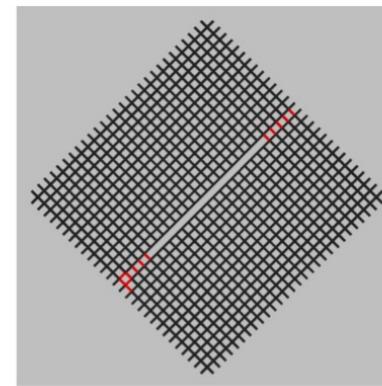
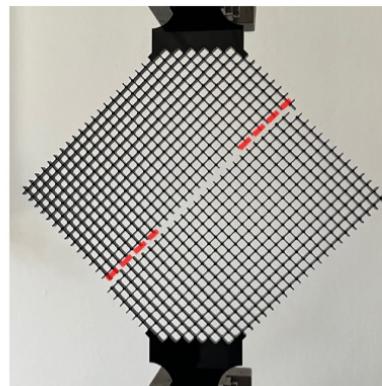
Experimental validation

Tension and shear

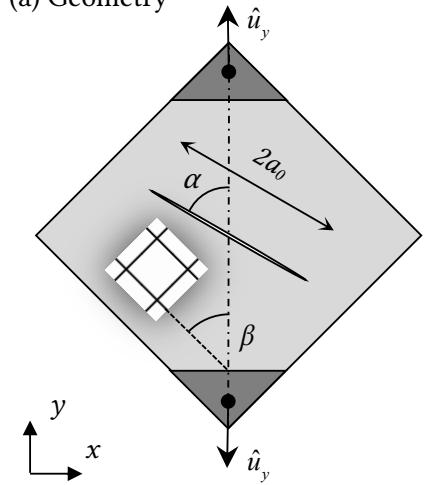
y
 x



Case 1.



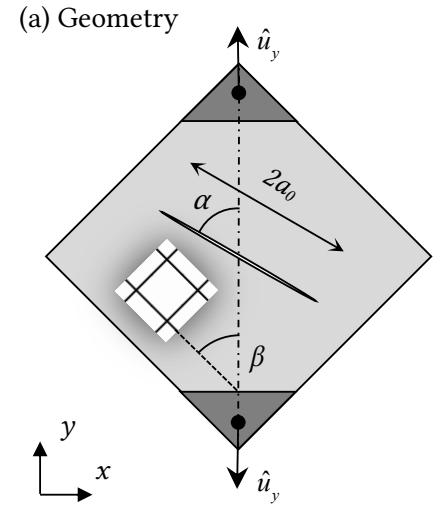
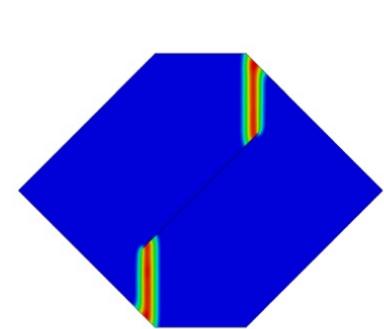
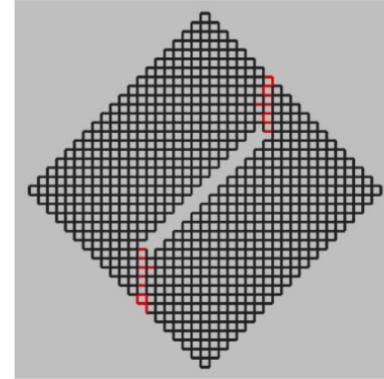
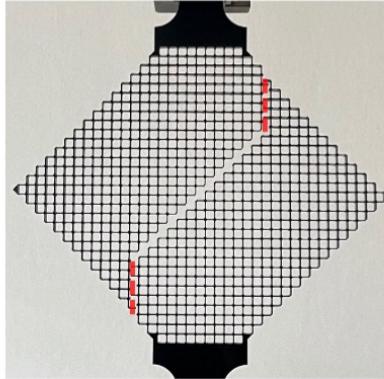
(a) Geometry



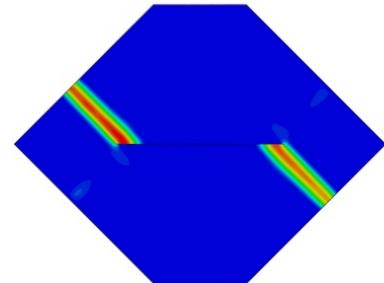
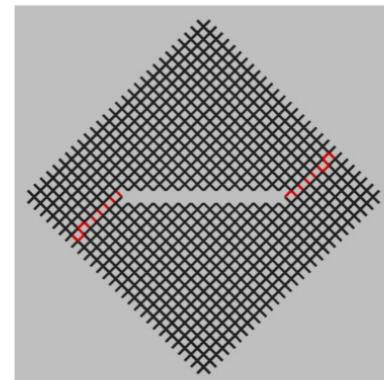
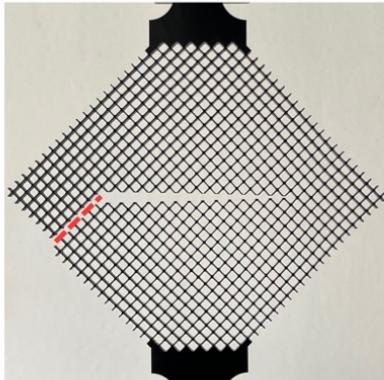
Experimental validation

Tension and shear

Case 3.



Case 4.

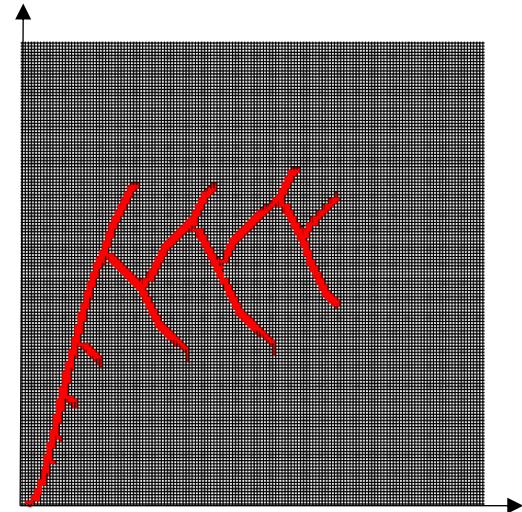


Conclusion / Perspectives

Fracture in periodic beam lattices

- **Toughness** can be defined
- Follows **continuum** theories
- **Homogenization**
 - Cosserat continuum
 - Multiple damage variables
 - Anisotropic phase-field

$$G^M \sim g_{\text{Irwin}} \approx \frac{(\sigma_c^m)^2 h^m}{E}$$



Other lattice types, 3D, etc...

Thank you for your attention

Try it out!

G. Molnár et al., Thermodynamically consistent linear-gradient damage model in Abaqus,
Engineering Fracture Mechanics, 108390, 2022.

G. Molnár & J. Réthoré, Fracture Toughness of Periodic Beam Lattices, **Journal of
Theoretical, Computational and Applied Mechanics** (submitted, 2024) [hal-04793587](https://hal.archives-ouvertes.fr/hal-04793587)

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